

A Thermodynamic Database for AlCl_3 -based Molten Salt Systems

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Chloroaluminate melts can be used as electrolytes for the production of aluminum and they are also involved in high energy density batteries ("Zebra" battery) : $\text{Na}/\beta\text{-Al}_2\text{O}_3/\text{NaAlCl}_4$, FeCl_2 , Fe. Molten chlorides have many other industrial applications. For example, transition-metal chlorides are involved in the hot corrosion of metallic alloys. They are also used in the production of magnesium by electrolysis : the electrolyte is $\text{NaCl-KCl-MgCl}_2\text{-CaCl}_2$ and the transition-metal chlorides (mostly MnCl_2 and FeCl_2) are dissolved impurities.

A thermodynamic database has been developed for the $\text{LiCl-NaCl-KCl-MgCl}_2\text{-CaCl}_2\text{-MnCl}_2\text{-FeCl}_2\text{-FeCl}_3\text{-CoCl}_2\text{-NiCl}_2\text{-AlCl}_3$ system. All binary subsystems (except $\text{AlCl}_3\text{-FeCl}_3$) as well as all higher order (mostly ternary) subsystems for which experimental data were available have been considered. A complete critical evaluation of all available phase diagram and thermodynamic data (enthalpy of mixing, emf and vapor pressure measurements) has been performed for all condensed phases (liquid, solid solutions, stoichiometric compounds) and relevant gaseous species, and optimized model parameters have been found which best reproduce all the data simultaneously. In this way the data have been rendered self-consistent, discrepancies among the data have been identified, and extrapolations and interpolations have been performed. The models can be used with Gibbs free energy minimization software to calculate phase diagram sections, vapor pressures, and all thermodynamic properties at all compositions over extended ranges of temperature and pressure.

The thermodynamic optimizations of the $\text{LiCl-NaCl-KCl-MgCl}_2\text{-CaCl}_2$ [1] and $\text{NaCl-KCl-MgCl}_2\text{-CaCl}_2\text{-MnCl}_2\text{-FeCl}_2\text{-CoCl}_2\text{-NiCl}_2$ [2a,2b] systems have been published. The liquid solution was modeled using the Modified Quasichemical Model [3,4] which takes into account short-range ordering between second-nearest-neighbor cations. All relevant solid solutions were modeled using appropriate models. In particular, the $\text{MgCl}_2\text{-MnCl}_2\text{-FeCl}_2\text{-CoCl}_2\text{-NiCl}_2$ solid solution [2a,2b] was modeled using a cationic substitutional model with an ideal entropy and an excess Gibbs free energy expressed as a polynomial in the component mole fractions. The $(\text{Li,Na,K})(\text{Mg,Ca,Mn,Fe,Co,Ni})\text{Cl}_3$ and the $(\text{Li,Na,K})_2(\text{Mg,Mn,Fe,Co,Ni})\text{Cl}_4$ solid solutions were modeled using the Compound Energy Formalism [5].

Recently, the thermodynamic database for the $\text{LiCl-NaCl-KCl-MgCl}_2\text{-CaCl}_2\text{-MnCl}_2\text{-FeCl}_2\text{-CoCl}_2\text{-NiCl}_2$ system was extended with the addition of AlCl_3 , and the thermodynamic optimization of the NaCl-KCl-AlCl_3 system was published [2c]. The binary systems AlCl-AlCl_3 (where $A = \text{Li, Na and K}$) show strong negative deviations from ideality at the equimolar composition (due to short-range ordering in the liquid phase), and the binary mixtures exhibit a region of liquid-liquid immiscibility at high AlCl_3 content. This is illustrated for the NaCl-AlCl_3 system in Figure 1, where the calculated phase diagram is compared with the available experimental data. The existence in AlCl-AlCl_3 melts of the AlCl_4^- and Al_2Cl_7^-

species has been observed by Raman spectroscopy [6,7]. In order to introduce two different compositions of maximum short-range-ordering near the AlCl_4^- and Al_2Cl_7^- compositions, pure liquid aluminum chloride was modeled as a mixture of AlCl_3 and Al_2Cl_6 (with paired aluminum cations). Similarly, the $\text{AlCl}_3\text{-MCl}_2$ systems (where $M = \text{Mg, Mn, Fe, Co and Ni}$) were modeled by introducing two different compositions of maximum short-range-ordering near the $M(\text{AlCl}_4)_2$ and $M(\text{Al}_2\text{Cl}_7)_2$ compositions. Satisfactory results were obtained in multi-component systems. This is illustrated in Figure 2, where the calculated section of the $\text{NaCl-KCl-MgCl}_2\text{-AlCl}_3$ phase diagram at constant weight ratio $\text{NaCl/KCl/MgCl}_2 = 74.0/19.3/6.7$ is compared with the available experimental data.

References

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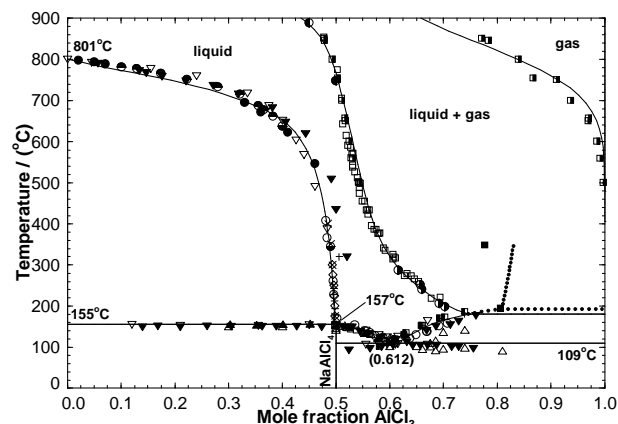


Figure 1 : Calculated NaCl-AlCl_3 phase diagram at 1 bar (dotted lines are liquid-liquid miscibility gap boundary and monotectic at $P > 1$ bar).

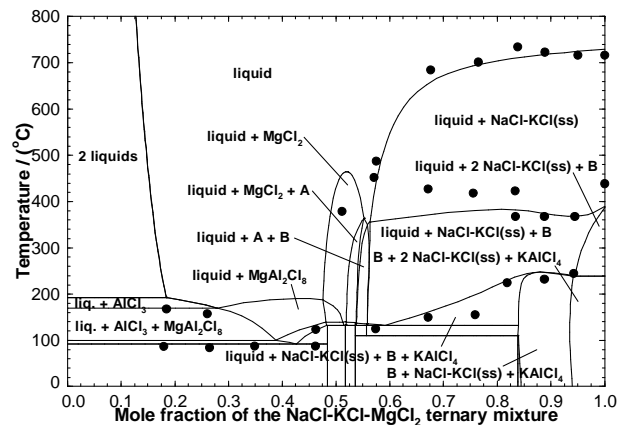


Figure 2 : Calculated section of the $\text{NaCl-KCl-MgCl}_2\text{-AlCl}_3$ phase diagram at constant weight ratio $\text{NaCl/KCl/MgCl}_2 = 74.0/19.3/6.7$ [$A = (\text{Na,K})\text{MgCl}_3(\text{ss})$ and $B = (\text{Na,K})_2\text{MgCl}_4(\text{ss})$].