

Water Vapor Effect on the Lattice Parameters of the Thermally Grown Oxides on Hot Work Tool Steels  
P. Bruckel, P. Lamesle, P. Lours, B. Pieraggi  
CROMeP, Research Center on Tools, Materials and Processes,  
Ecole des Mines d'Albi-Carmaux, 81013 Albi, France

Hot work tool steels containing about 5wt% chromium are commonly used in forging processes. They may suffer chemical damage during service since the oxide films formed on their surface are not protective [1]. Although some data on the oxidation of Fe-Cr alloys with a low chromium content in oxygen or air are available in the literature [2-3], these results rarely mention the effect of the water vapor on the oxidation mechanisms [4].

The purpose of this work is to determine the lattice parameter evolution for different  $\text{Fe}_2\text{O}_3\text{-Cr}_2\text{O}_3$  solid solutions developed in either an oxygen containing media or in an ' $\text{O}_2+\text{H}_2\text{O}$ ' containing one. The investigated temperatures are  $600^\circ\text{C}$  and  $700^\circ\text{C}$  for exposure times of 90 hours. X-Ray diffraction is used in the Grazing Incidence configuration to characterize the thermally grown oxides. The diffracted response (figure 1) exhibits peaks shifted from the theoretical position of pure  $\alpha\text{-Fe}_2\text{O}_3$  and pure  $\text{Cr}_2\text{O}_3$ . This is particularly interesting since this typical peak shift can be correlated to the lattice parameters of the oxide expressed as  $\text{Fe}_{2-x}\text{Cr}_x\text{O}_3$ .

For the evaluation of parameter  $x$ , the  $\text{M}_2\text{O}_3$  oxides parameters are taken in the hexagonal system and the position of the  $(hkl)$  diffraction peak is measured on the experimental pattern. Our results will focus on the  $(300)$  peak as the  $d_{hkl}$  expression in the hexagonal system can be simplified this way. Pure  $\alpha\text{-Fe}_2\text{O}_3$  and  $\text{Cr}_2\text{O}_3$  are considered to be the limits of our system and correspond respectively to  $x = 0$  and  $x = 2$ . Their lattice parameters are given in table 1. A first assumption is that the evolution of parameter ' $a_H$ ' is linear from pure hematite to pure chromite lattice. This seems to be in good agreement with the results reported by Di Cerbo *et al.* [5] and by Wretblad [6] expressed in function of the amount of  $\text{Cr}_2\text{O}_3$  in the solid solution (figure 2).

Finally, the evolution of the lattice parameter ' $a_H$ ' at  $600^\circ\text{C}$  when for example 11 vol% of  $\text{H}_2\text{O}$  are added to the ' $\text{O}_2$ ' atmosphere shows an increase from 5.0299 ( $x=0.12$ ) to 5.0337 ( $x=0.04$ ) respectively. The corresponding amounts of diluted chromite are 6wt% and 2 wt%.

[1] P. BRUCKEL, P. LOURS, P. LAMESLE, B. PIERAGGI – 5<sup>th</sup> International Conference on the Microscopy of Oxidation – Limerick, Ireland – July 26/28<sup>th</sup>, 2002 – to be published in *Materials at High Temperatures*

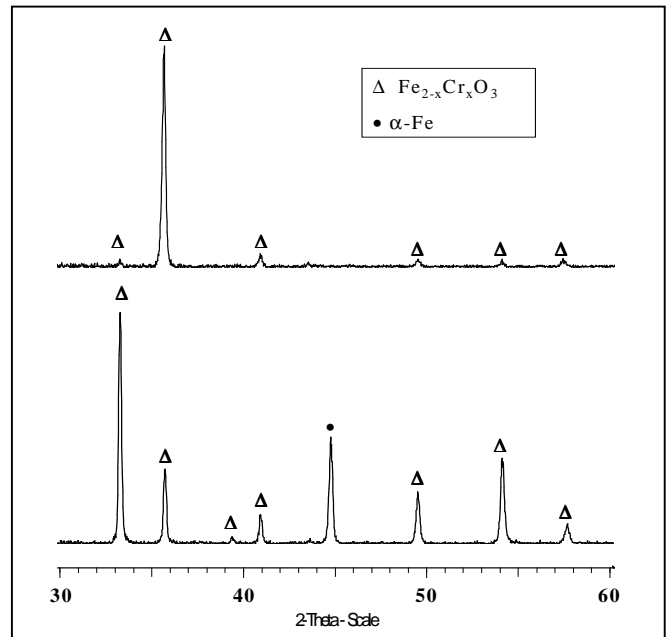
[2] H.J. YEARIAN, E.C. RANDELL, T.A. LONGO – Corrosion (Houston, Texas), vol. 12, 1956, p. 515T

[3] D. MORTIMER, W.B.A. SHARP – British Corrosion Journal, vol. 3, 1968, p. 61

[4] C.T. FUJII, R.A. MEUSSNER – Corrosion of Iron and Steel, vol. 111, n° 11, 1964, p. 1215

[5] R.K. Di CERBO, A.U. SEYBOLT – Journal of the American Ceramic Society, vol. 42, 1959, p. 430

[6] P.E. WRETLAD – Ceramic Abstracts, vol. 9, n° 10, 1930, p. 881



**Figure 1 :** XRD patterns for the grazing angle  $5^\circ$  after 90 hours exposure at  $600^\circ\text{C}$  (a) in the  $\text{O}_2$  containing atmosphere, (b) in the ' $\text{O}_2 + 11 \text{ vol}\% \text{H}_2\text{O}$ ' gas mixture.

**Table 1 :** Lattice parameters of  $\alpha\text{-Fe}_2\text{O}_3$  and  $\text{Cr}_2\text{O}_3$  in the hexagonal system taken from the JCPDS cards number 33-664 and 84-313 respectively, and from reference [5].

	$\text{Fe}_2\text{O}_3$	$\text{Cr}_2\text{O}_3$
$a_H$ (a.u.)	5.0356	4.9372
$c_H$ (a.u.)	13.7489	13.53
$a_H$ (a.u.) from ref. [5]	5.0343	4.9591
$c_H$ (a.u.) from ref. [5]	13.749	13.599

**Figure 2 :** Evolution of the lattice parameter ' $a_H$ ' in the solid solutions  $\text{Fe}_{2-x}\text{Cr}_x\text{O}_3$ .

