## Effect of Metal Loading on H<sub>2</sub> Sensing Properties of SnO<sub>2</sub> Modified with Mesoporous SnO<sub>2</sub>

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In order to clarify the effect of metal loading on the H<sub>2</sub> sensing properties of thick film semiconductor gas sensors, several SnO<sub>2</sub>-based powders have been prepared and tested. SnO<sub>2</sub> powder was prepared by calcination of tin oxalate at 600°C for 5 h. Loading of 0.5 wt% Ru or Pd on the SnO<sub>2</sub> (0.5M/SnO<sub>2</sub>, M = Ru or Pd) powder was conducted by a conventional method. Procedure of surface modification of the SnO<sub>2</sub> powder with a mesoporous SnO<sub>2</sub> (m-SnO<sub>2</sub>) layer has been described elsewhere.<sup>1)</sup> Response of the sensors was measured to 1000 ppm H<sub>2</sub> in air at 250-550°C. Magnitude of the response was defined as the ratio ( $R_a/R_g$ ) of sensor resistance in air ( $R_a$ ) to that ( $R_g$ ) in 1000 ppm H<sub>2</sub> balanced with air.

Figure 1 compares the H<sub>2</sub> sensing properties of thick film sensors (film thickness: ca.  $30-40 \ \Box m$ ) prepared with several SnO<sub>2</sub>-based powders. The surface modification with an m-SnO<sub>2</sub> layer led to improvement of H<sub>2</sub> response in the temperature range studied, and the improvement became remarkable by the repetition (see the data for m-SnO<sub>2</sub>(2)/SnO<sub>2</sub>). Loading of Ru or Pd on the SnO<sub>2</sub> powder was also effective, especially at lower temperatures than 400°C. The improvement induced by the surface modification may be explained by diffusion control of gaseous O<sub>2</sub>, while that induced by the loading by the chemical sensitization effect.

More significant improvement in H2 response could be achieved with the twice surface modification of  $0.5 \text{Ru}/\text{SnO}_2$  (see the data for m-SnO<sub>2</sub>(2)/(0.5 \text{Ru}/\text{SnO}\_2)), as shown in Fig. 2, whereas the Ru loading after the surface modification (see the data for 0.5Ru/m-SnO<sub>2</sub>(2) /SnO<sub>2</sub>) resulted in comparable response with that for a unloaded sensor. In contrast, the maximum H<sub>2</sub> response was ca. 25 at most in the case of  $m-SnO_2(2)/(0.5Pd$ Thus, the  $m-SnO_2(2)/(0.5Ru/SnO_2)$  sensor  $/SnO_2$ ). exhibited the highest H<sub>2</sub> response among the sensors studied. But, the sensor showed rather slow recovery, whereas its response was very fast. These results suggest that the markedly improved response of the m-SnO<sub>2</sub>(2)/(0.5Ru/SnO<sub>2</sub>) sensor arises from a synergy effect of the diffusion control and the chemical sensitization. The Ru loading after the surface modification may reduce the permeation amount of H<sub>2</sub> into the SnO<sub>2</sub> surface, and the Pd loading before and after the surface modification may induce a similar result due to higher catalytic activity than Ru.

 T. Hyodo, S. Abe, Y. Shimizu, M. Egashira, *Sens. Actuators B*, **93**, 590 (2003).

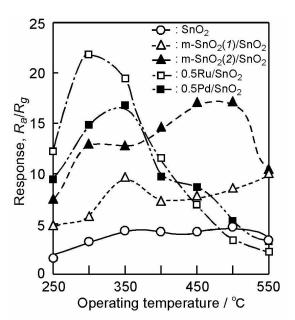


Fig. 1 Operating temperature dependence of response of sensors to  $1000 \text{ ppm H}_2$ .

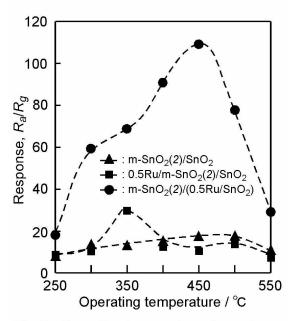


Fig. 2 Operating temperature dependence of response of sensors to 1000 ppm  $H_2$ .

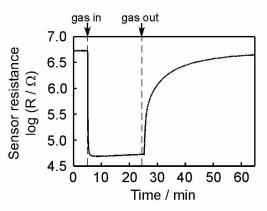


Fig. 3 Response transient of m-SnO<sub>2</sub>(2)  $/(0.5Ru/SnO_2)$  to 1000 ppm H<sub>2</sub> at 450°C.